

# ELDORA TPARC/TCS08 Dataset

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NCAR                                    NCAR/NPS

<http://www.eol.ucar.edu/instrumentation/airborne-instruments/eldora/eldora-help-center>

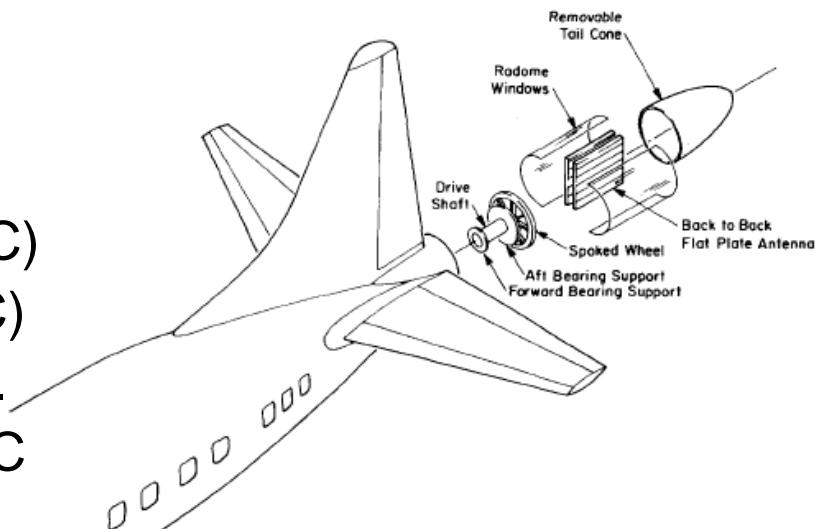
# ELDORA

## Airborne

# Doppler Radar



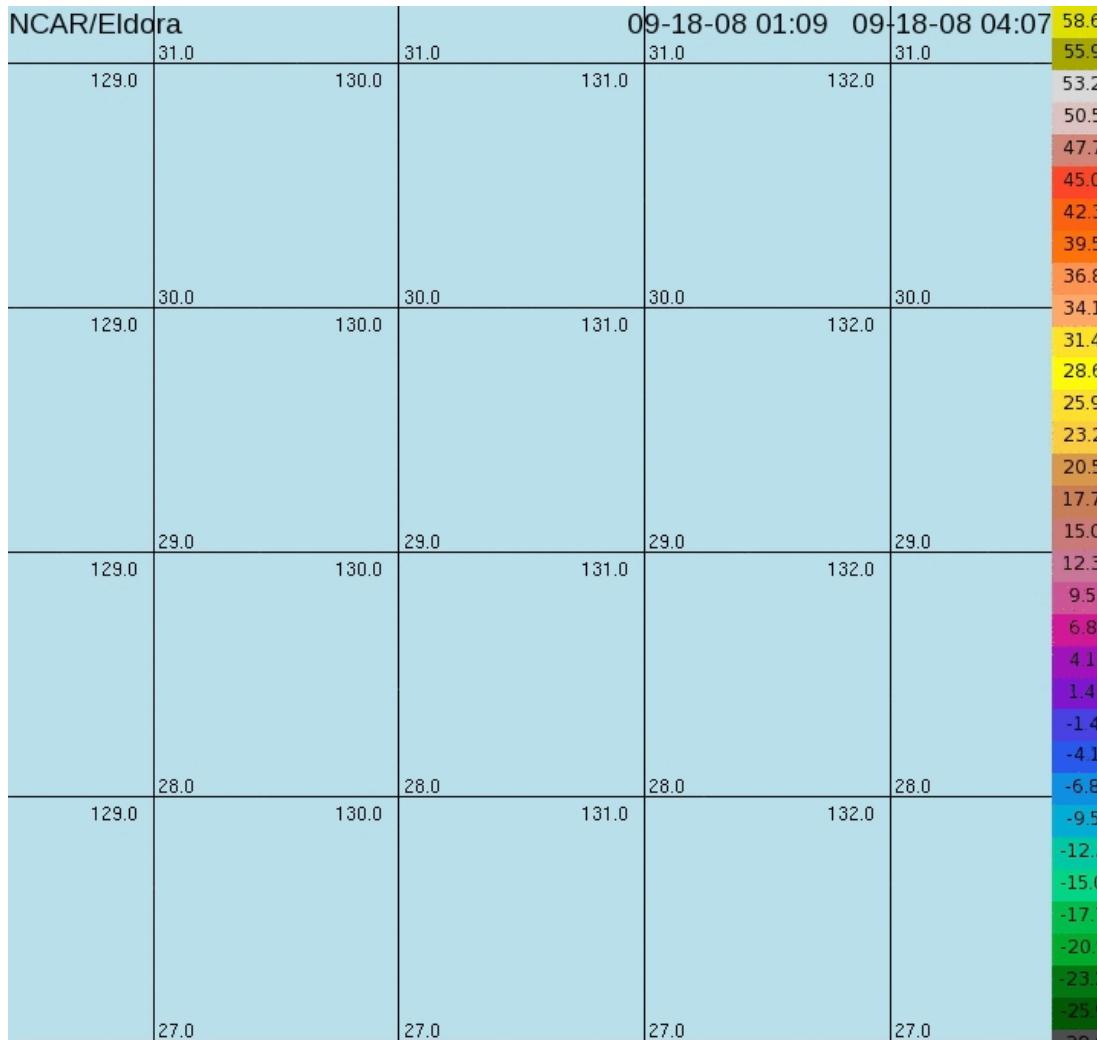
- ~~NRL-P3 E~~lectra DOppler RAdar
  - 3.2 cm, 1.8° beam, 38.7 dB Gain
  - 2 Antennas & Tx
  - 40 kW Peak Power
  - 2 PRF in 4:5 ratio (62 m/s NV in TPARC)
  - Scan rate up to 144°/s (87°/s in TPARC)
  - Complex 'chirp' w/4 (3 in TPARC) Freq.
  - ~500 m along track resolution in TPARC
  - Unambig. Range ~75 km (Convective)
- TOGA COARE (93), VORTEX 95, FASTEX (97), LAKEICE (97/98), MAP (99), IHOP (02), CRYSTALFACE (02), BAMEX (03), RAINEX (05), TCS-08/TPARC (08)



# ELDORA Data Fields

Field Name	Description
DBZ	Radar Reflectivity
VG	Ground-relative, navigation corrected, Doppler velocity
NCP	Normalized Coherent Power
SW	Spectrum Width
VT	VG thresholded with NCP below 0.25
VS	Short-pulse Doppler velocity
VL	Long-pulse Doppler velocity
VR	Aircraft-relative Doppler velocity

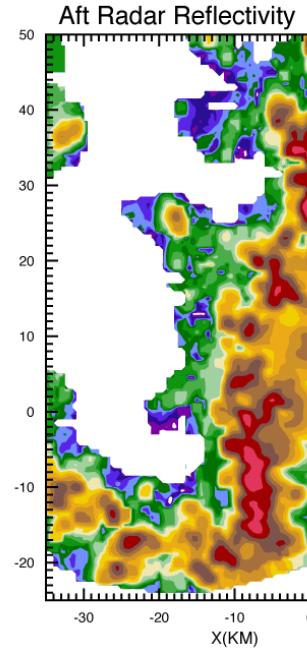
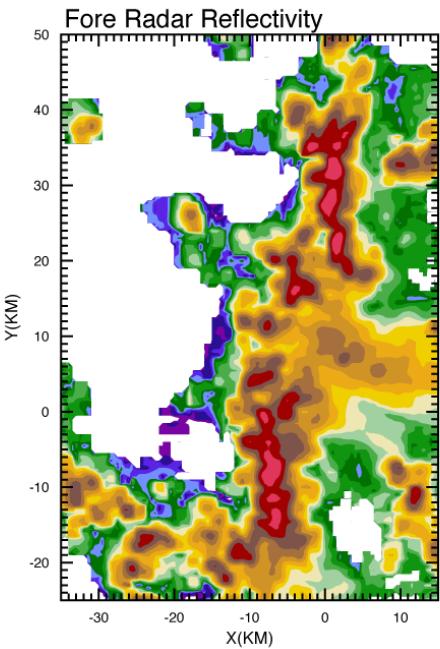
# CAPPI Movies Bonus Dataset



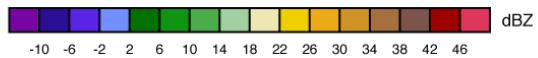
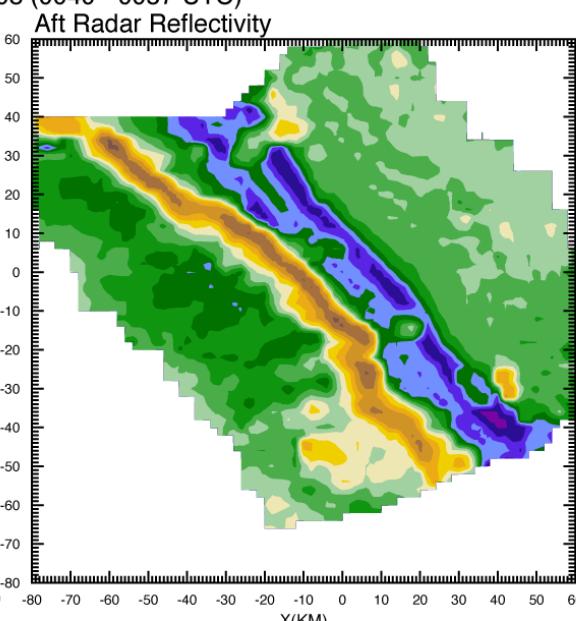
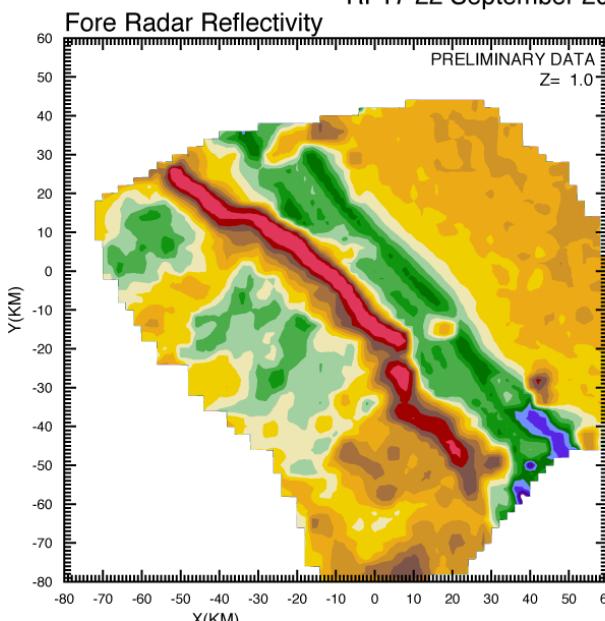
# Dataset Summary

- Velocity data appears very good throughout project
- INS Navigation corrections were stable
- Aft Reflectivity is low from RF16 – RF21, reduced sensitivity in cloudy & clear air
- 165 GB dataset ready, on CODIAC soon
  - Dorade sweep files in ~200 MB 10-minute tar files (netCDF translator available)
  - Navigation correction factors (cfac files)

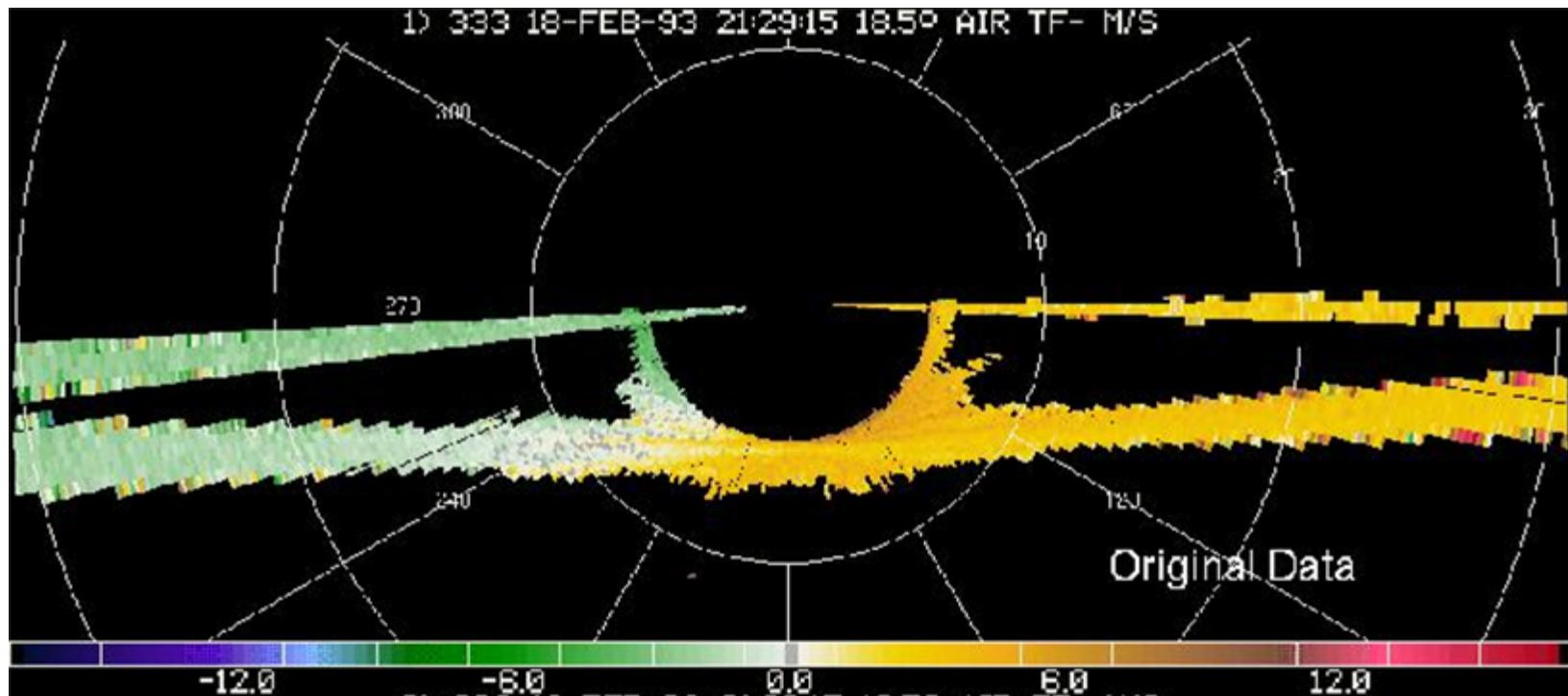
RF11 14 September 0037 - 0048 UTC



RF17 22 September 2008 (0040 - 0057 UTC)



# Problems in Raw Data



1. Earth surface is tilted.
2. Earth surface is not stationary.
3. Earth surface moves at different speeds.

Testud et al 1995

# ELDORA Navigation Corrections

- Accurate knowledge of the aircraft orientation and radar beam pointing angle is essential to airborne Doppler analysis

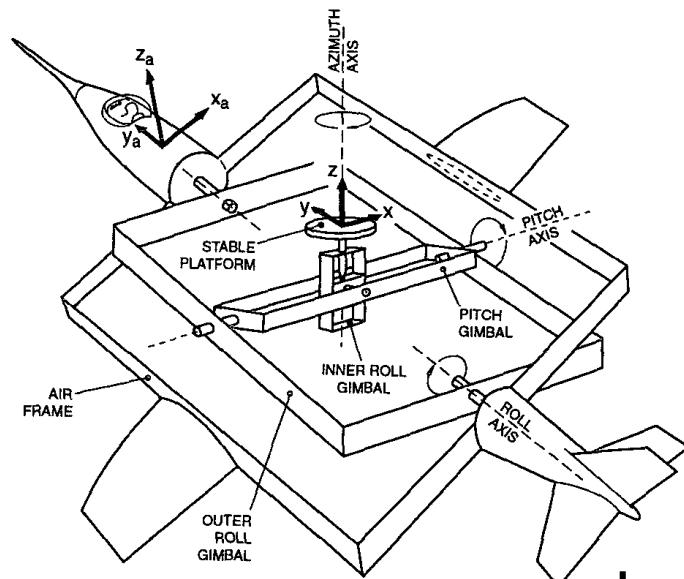
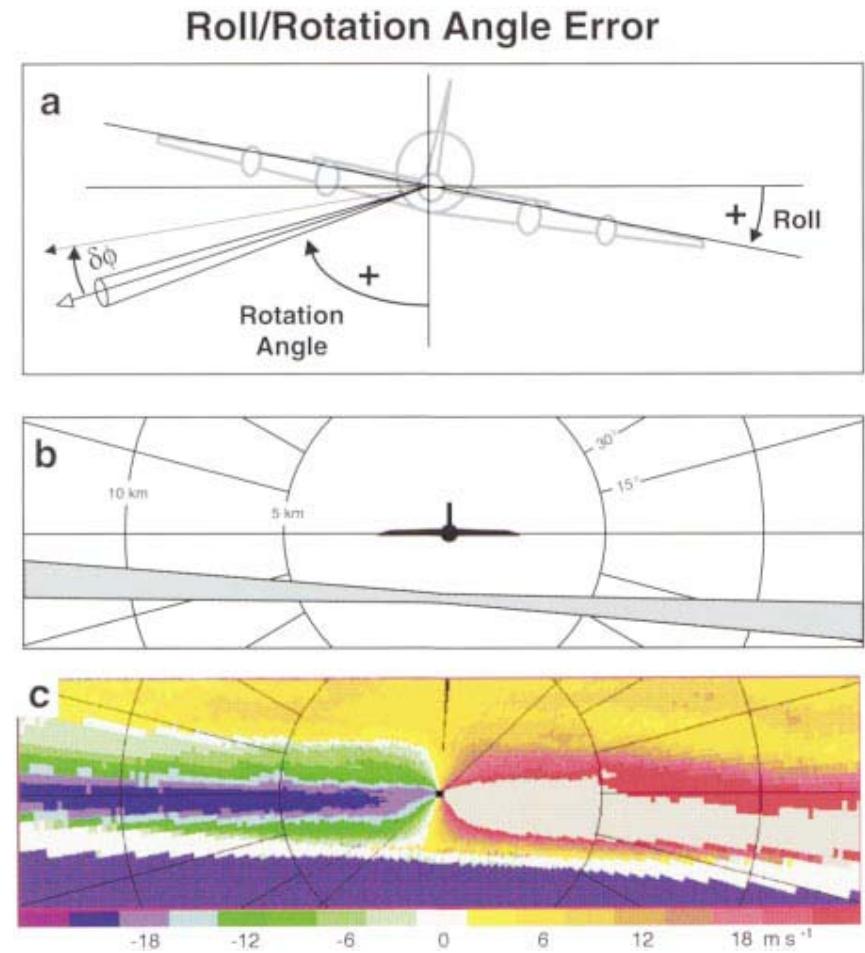


FIG. 1. Platform gimbals and reference frame  
[adapted from Axford (1968)].



Lee et al, 1994; Testud et al, 1995;  
Georgis et al, 2000; Bosart et al, 2002

# Definitions of INS Attitude Angles

- Meteorological coordinates-positive clockwise
- Drift is the angle between track and heading ( $T=H+D$ ), a positive drift angle is defined as the track is more clockwise than the heading
- Pitch is the angle that the aircraft longitudinal axis makes with the horizontal plane, nose up is positive pitch
- Roll is the angle that the wings make with the horizontal plane, right wing down is positive
- Through these three sequential rotation, **X is transformed into  $X_a$**

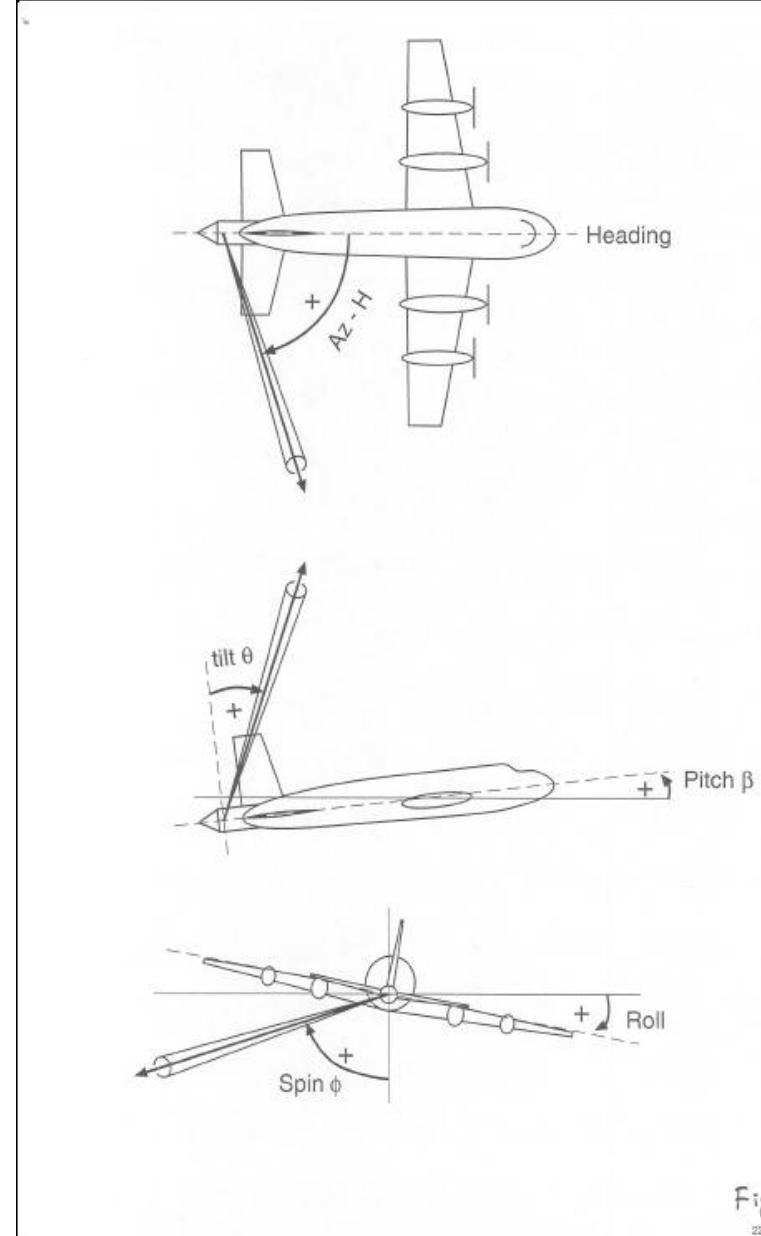


Figure 2b

# Uncertainties in INS and Antenna Pointing Angles

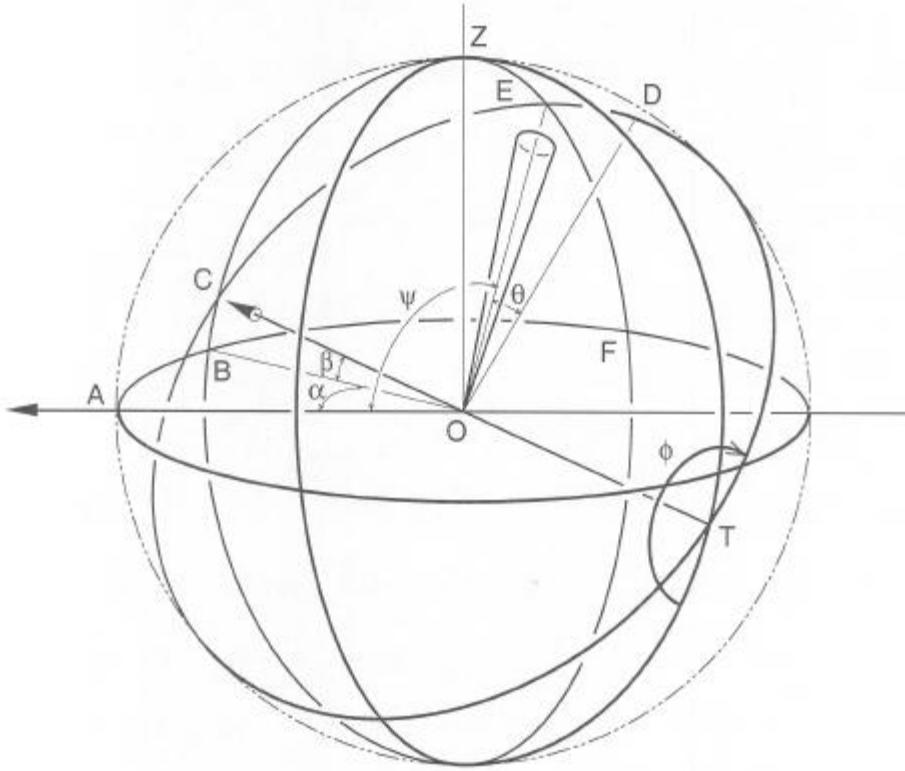
Measurement/Instrument Errors:

- Horizontal velocity ( $V_H$ ):  $\pm 2 \text{ m s}^{-1}$
- Drift angle ( $\alpha$ ):  $\pm 1^\circ$
- Aircraft vertical velocity ( $W$ ):  $\pm 0.15 \text{ m s}^{-1}$
- Pitch angle ( $\beta$ ):  $\pm 0.05^\circ$
- Tilt angle ( $\theta$ ):  $\pm 0.05^\circ$
- Roll/spin angle ( $\phi$ ):  $\pm 0.05^\circ$

Systematic errors (e.g., mounting errors) in the order of  $1^\circ$  may exist

# Spherical Trigonometry and Radial Velocity

$$V_r = u \sin(A_z) \cos(EL) + v \cos(A_z) \cos(EL) + (w + w_t) \sin(EL) - V_g - V_a$$



$\alpha$ : drift  
 $\beta$ : pitch  
 $\phi$ : spin/rotation

$\theta$ : tilt  
 $\Psi$ :  $\pi/2$ -track-relative tilt  
 $A_z$ : azimuth  
 $EL$ : elevation

$$\cos A_z = \frac{\sin \theta - \sin EL \sin \beta}{\cos EL \cos \beta}$$

$$\sin EL = \sin \theta \sin \beta - \cos \theta \cos \beta \cos \phi$$

$$\cos \Psi = \cos \alpha \cos \beta \sin \theta - \cos \alpha \sin \beta \cos \theta \cos \phi - \sin \alpha \cos \theta \sin \phi$$

# Velocity Error Analysis

Estimated aircraft ground speed ( $V_{Ge}$ ):

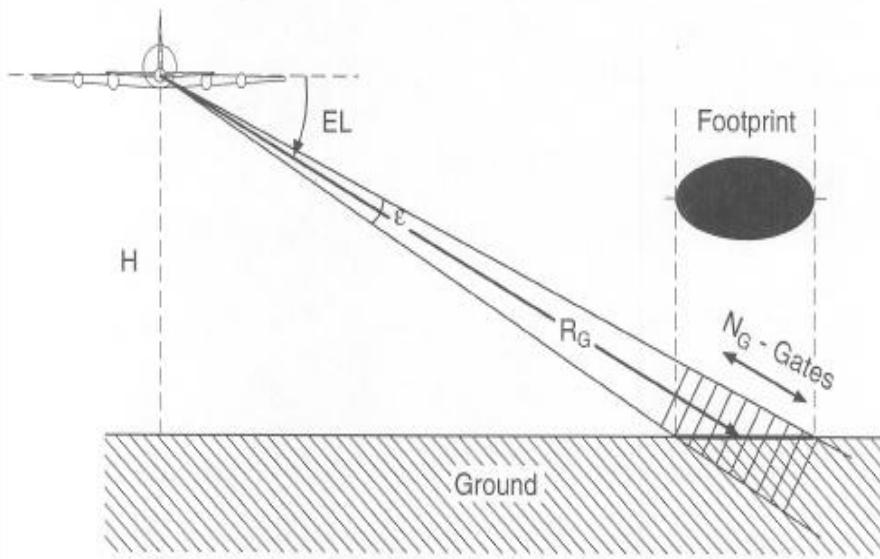
$$\begin{aligned} V_{Ge} &= V_H \cos \Psi - W \sin EL \\ &= (-V_H + V_o \cos \lambda_o) (\cos \alpha \cos \beta \sin \theta \\ &\quad + \cos \alpha \sin \beta \cos \theta \cos \phi - \sin \alpha \cos \theta \sin \phi) \\ &\quad - W (\sin \theta \sin \beta - \cos \theta \cos \beta \sin \phi) \end{aligned}$$

Measured aircraft ground speed by the radar ( $V_G$ ):

$\delta V_G$ : the velocity of the ground gate after removing ground speed

$$\begin{aligned} \delta V_G &= V_G - V_{Ge} \\ &= \delta(-V_H \cos \Psi - W \sin EL) \\ &= \delta W \cos \theta \cos \phi - V_H (\cos \alpha \cos \theta + \sin \alpha \sin \theta \sin \phi) \delta \theta \\ &\quad + \delta \theta V_H \sin \alpha \cos \theta \cos \phi - \delta \beta V_H \cos \alpha \cos \theta \cos \phi \\ &\quad + V_H (\sin \alpha \sin \theta + \cos \alpha \cos \theta \sin \phi) \\ &\quad - (\cos \alpha \sin \theta - \sin \alpha \cos \theta \sin \phi) \delta V_H \\ &= A + B_1 \sin \phi + B_2 \cos \phi \end{aligned}$$

# Range Error Analysis



$$R_G = -\frac{H}{\sin EL}$$

$$N_G \approx \frac{R\varepsilon}{\delta R \tan EL}$$

$\delta R$ : gate spacing  
 $R_R$ : actual distance to the ground  
 $\varepsilon$ : beam width

$$R_G = -\frac{H \cos \phi}{\sin EL} = -\frac{H}{\sin \theta \sin \beta - \cos \theta \cos \beta \cos \phi} = R_R + \Delta R$$

$$R_{Ge} = -\frac{H_e}{\sin \theta_e \sin \beta_e - \cos \theta_e \cos \beta_e \cos \phi_e}$$

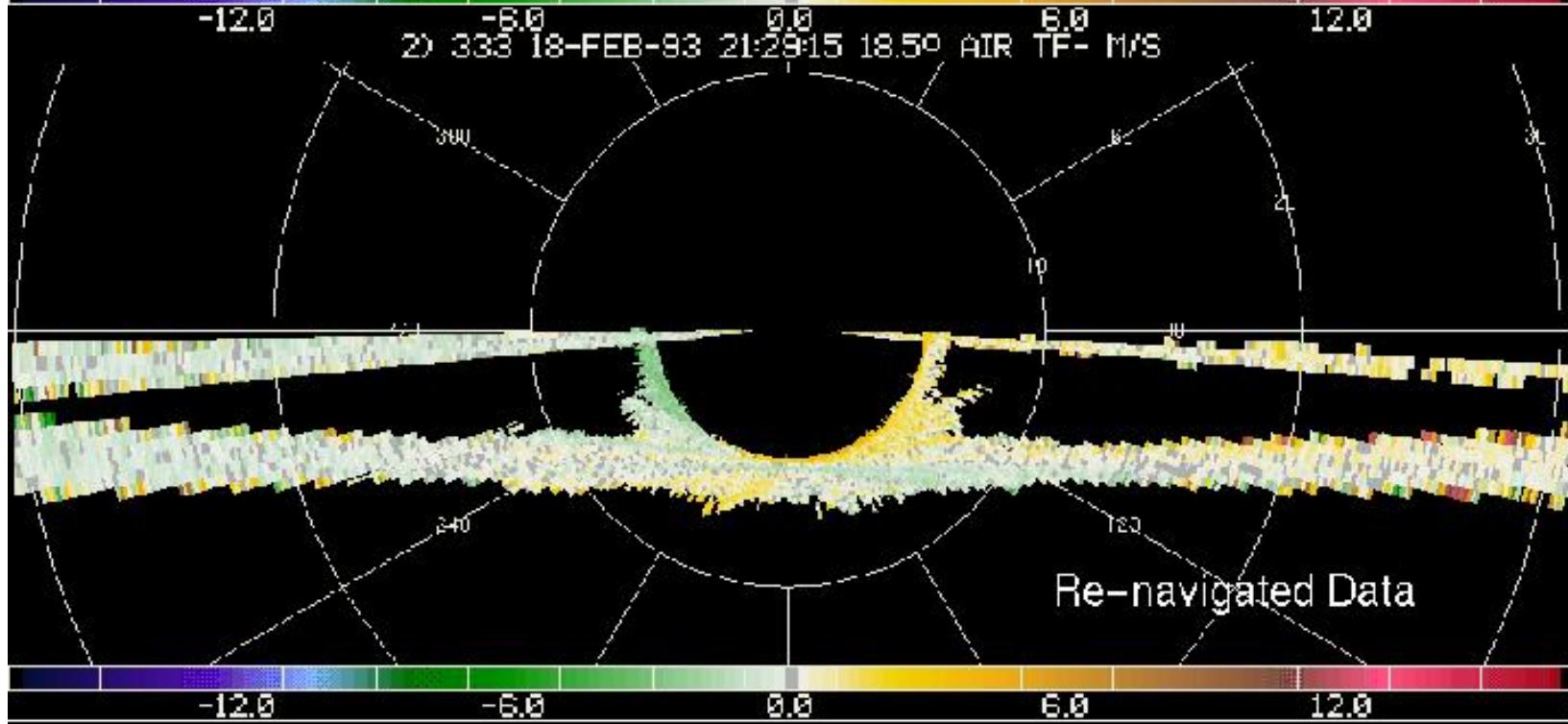
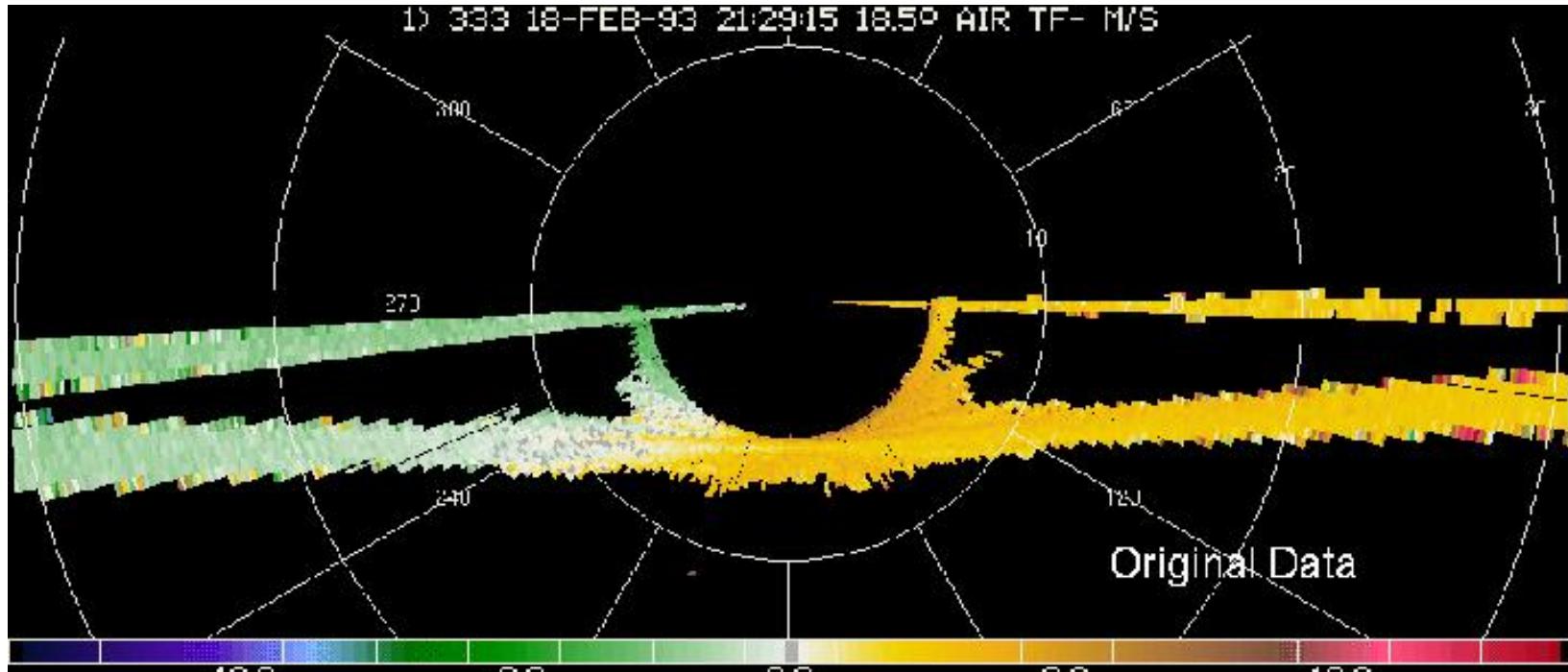
# Range Error Analysis (Continue)

$\delta R_G$ : difference between the actual distance to the ground and estimates from aircraft altitude and elevation angles of a radar beam

$$\begin{aligned}\delta R_G &= R_G - R_{Ge} \\ &= R_G \left( \frac{\delta H}{H} + \frac{\tan \theta}{\cos \phi} \delta \beta + \tan \theta \delta \theta + \tan \theta \delta \phi \right)\end{aligned}$$

$$R_R - R_{Ge} = \delta R_G - \Delta R$$

$$\begin{aligned}\cos^2 \phi (R_R - R_{Ge}) &= -\frac{\Delta R}{2} + \frac{H \tan \theta}{\cos \theta} \delta \beta + \left( \frac{H \delta \phi}{\cos \theta} \right) \sin \phi \\ &\quad + \left( \frac{\delta H + H \tan \theta \delta \theta}{\cos \theta} \right) \cos \phi - \frac{\Delta R}{2} \cos 2\phi \\ &= C + D_1 \sin \phi + D_2 \cos \phi + E \cos 2\phi\end{aligned}$$

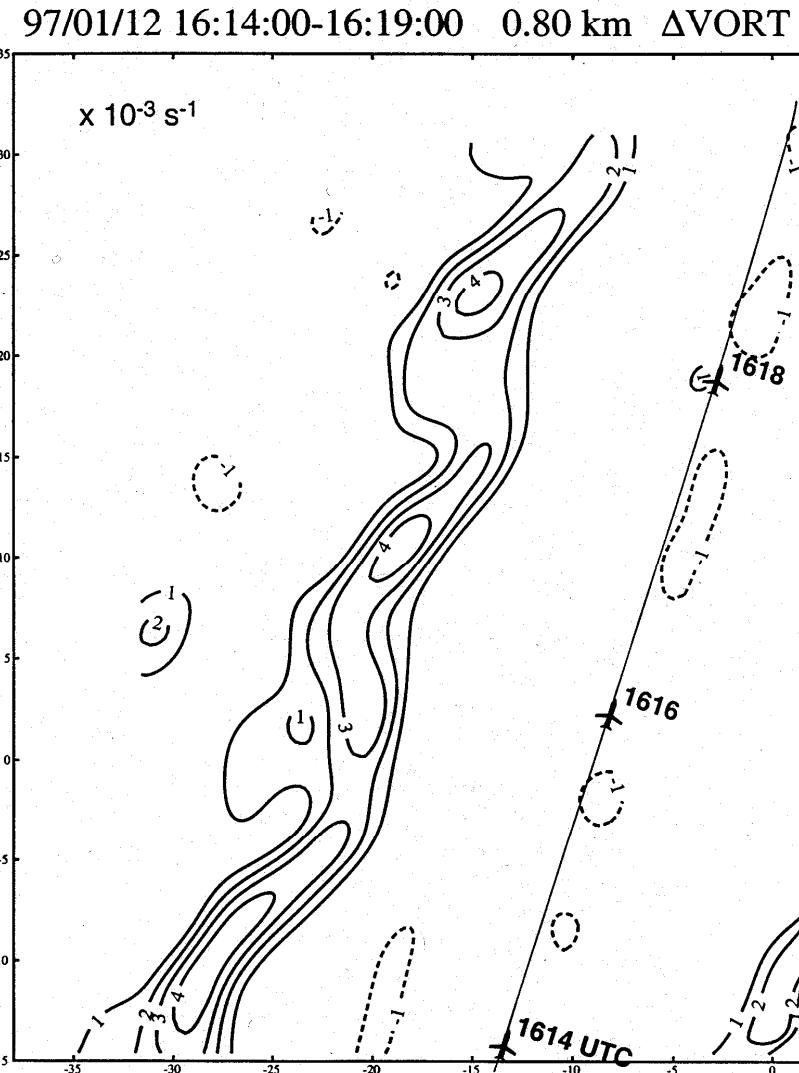


# Moving Ocean Surface

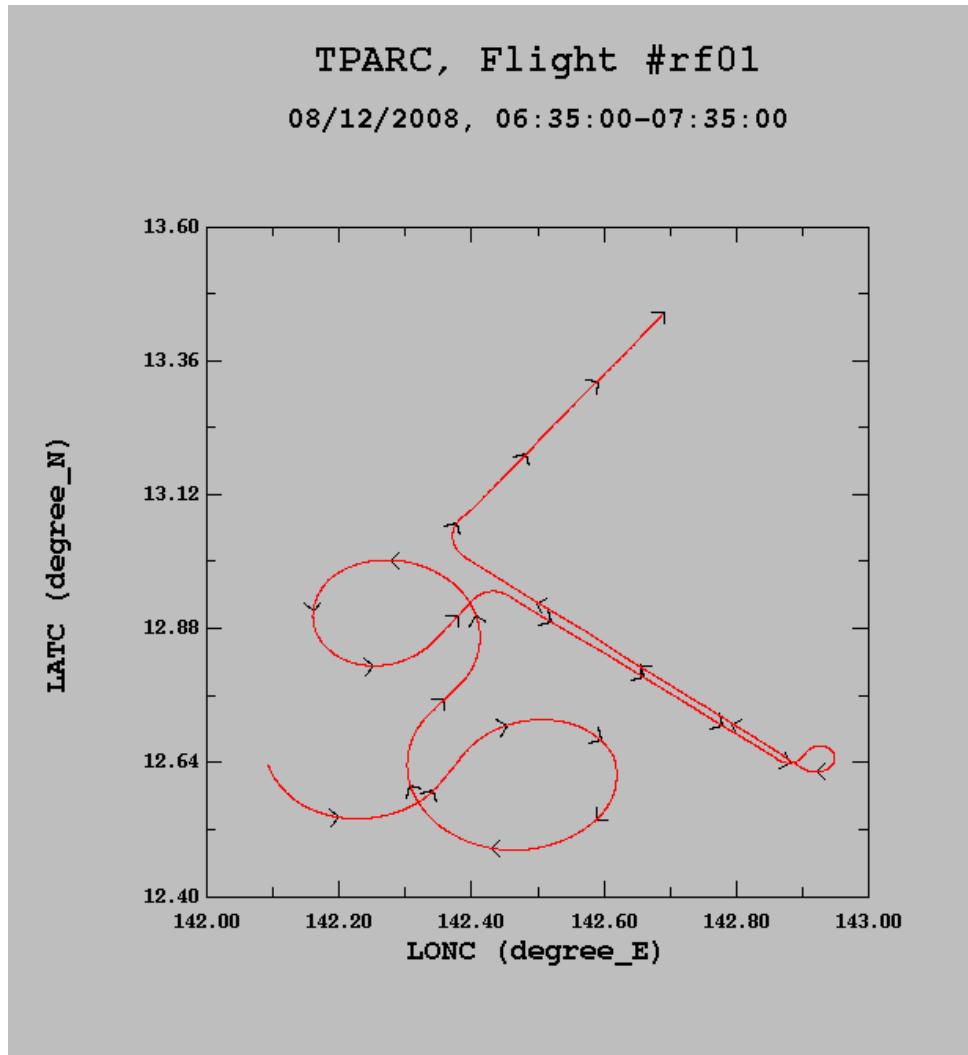
- If the ground is not stationary, then we match in situ wind with near aircraft dual-Doppler wind if there are scatterers near the aircraft (BLW correction)
- Use to refine ground speed and drift

Example:  
FASTEX IOP2 cold front case

VORTICITY DIFFERENCE  
(Navig Corr - NO Navig Corr)



# Reverse Headings



Research Flight	Date	Time	Range Fore	Range Aft	Altitude Corr	Pitch Corr	Rotation Aft	Rotation Fore
1	8/12/08	28:00.0	135.03	139	-0.036	-1.565	0.09	-0.17
2	8/16/08	08:00.0	122.28	120.38	-0.03	-1.575	0.03	-0.27
3	8/16/08	46:00.0	99.84	143.42	-0.053	-1.64	0.08	-0.22
4	8/18/08	49:00.0	84.26	175.26	-0.025	-1.605	0.02	-0.18
5	8/28/08	00:00.0	40	148.56	-0.013	-1.64	0.08	-0.11
6	8/29/08	43:00.0	41.29	156.29	-0.028	-1.585	0.05	-0.2
7	9/1/08	25:00.0	132.06	130.8	-0.039	-1.605	0.06	-0.18
8	9/8/08	12:00.0	125.63	202.43	-0.029	-1.625	0.09	-0.2
9	9/9/08	32:00.0	61.84	98.27	-0.031	-1.62	0.06	-0.23
10	9/11/08	00:00.0	165.28	151.09	-0.017	-1.63	-0.2	-0.47
11	9/13/08	20:00.0	126.73	146.37	-0.043	-1.645	-0.02	-0.34
12	9/14/08	20:00.0	88.62	84.66	-0.021	-1.63	-0.03	-0.32
13	9/17/08	40:00.0	38.15	171.38	-0.025	-1.635	-0.08	-0.33
14	9/18/08	10:00.0	134.1	163.38	-0.028	-1.645	-0.08	-0.38
15	9/19/08	30:00.0	159	145.24	-0.035	-1.61	-0.03	-0.37
16	9/20/08	16:00.0	66.5	196.3	-0.018	-1.64	-0.04	-0.33
17	9/22/08	15:00.0	168.96	156.46	-0.023	-1.645	-0.11	-0.39
18	9/23/08	06:00.0	79.65	209.02	-0.048	-1.615	-0.11	-0.32
19	9/24/08	15:00.0	89.18	120.33	-0.047	-1.625	-0.14	-0.33
20	9/25/08	27:00.0	94.17	90.62	-0.039	-1.58	-0.08	-0.36
21	9/27/08	12:00.0	46.47	192.2	-0.036	-1.62	-0.08	-0.33
22	10/2/08	27:00.0	164.69	184.85	-0.02	-1.63	-0.28	-0.51
23	10/4/08	35:00.0	94.07	205.96	-0.021	-1.66	-0.23	-0.53

# TPARC/TCS08 Corrections

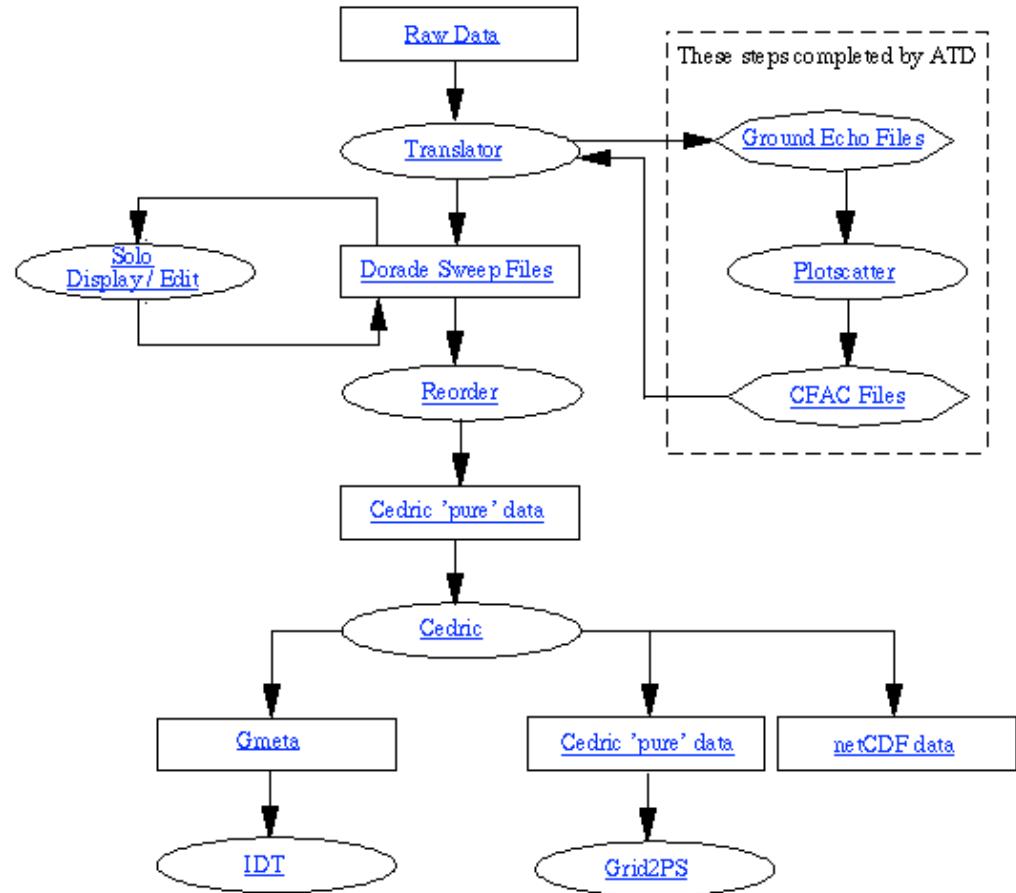
	Drift Corr	Ground Speed Reverse Legs	Tilt Aft	Tilt Fore
Mean	0.019565	0.88563	0.30053	-0.13158
Median	0.055	0.9275	0.3	-0.15
Std Deviation	0.49641	0.15072	0.060044	0.070179

- Ground speed, Tilt error determined from reverse headings, drift from project average

	Range Fore	Range Aft	Altitude Corr (km)	Pitch Corr	Rotation Aft	Rotation Fore
Mean	102.51	153.58	-0.030652	-1.6207	-0.041304	-0.30739
Median	94.17	151.09	-0.029	-1.625	-0.03	-0.33
Std Deviation	42.167	35.907	0.010731	0.024602	0.10559	0.1103

# Basic Analysis Process

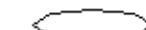
ELDORA DATA PROCESSING FLOW CHART



= Data Format



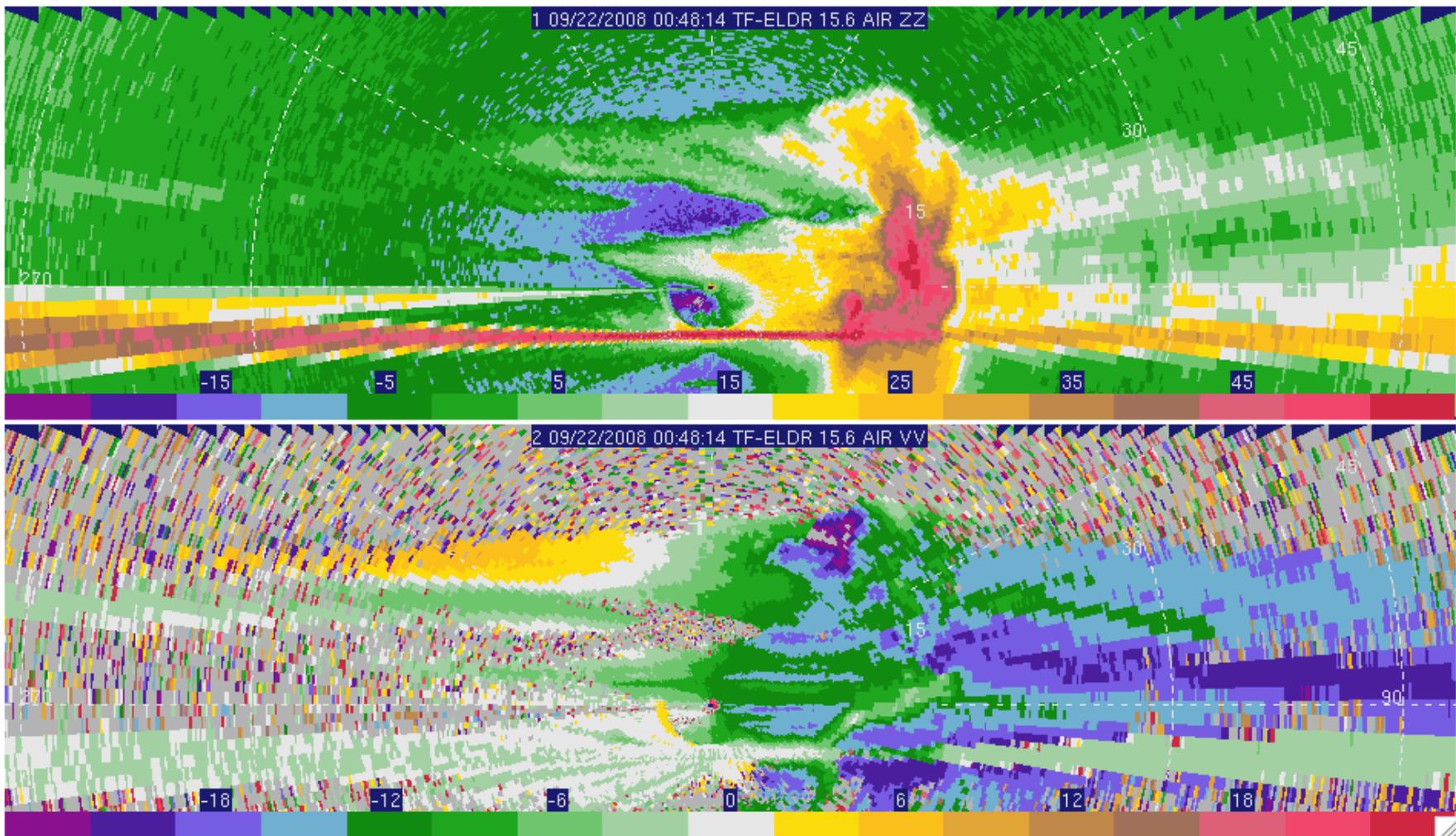
= Software



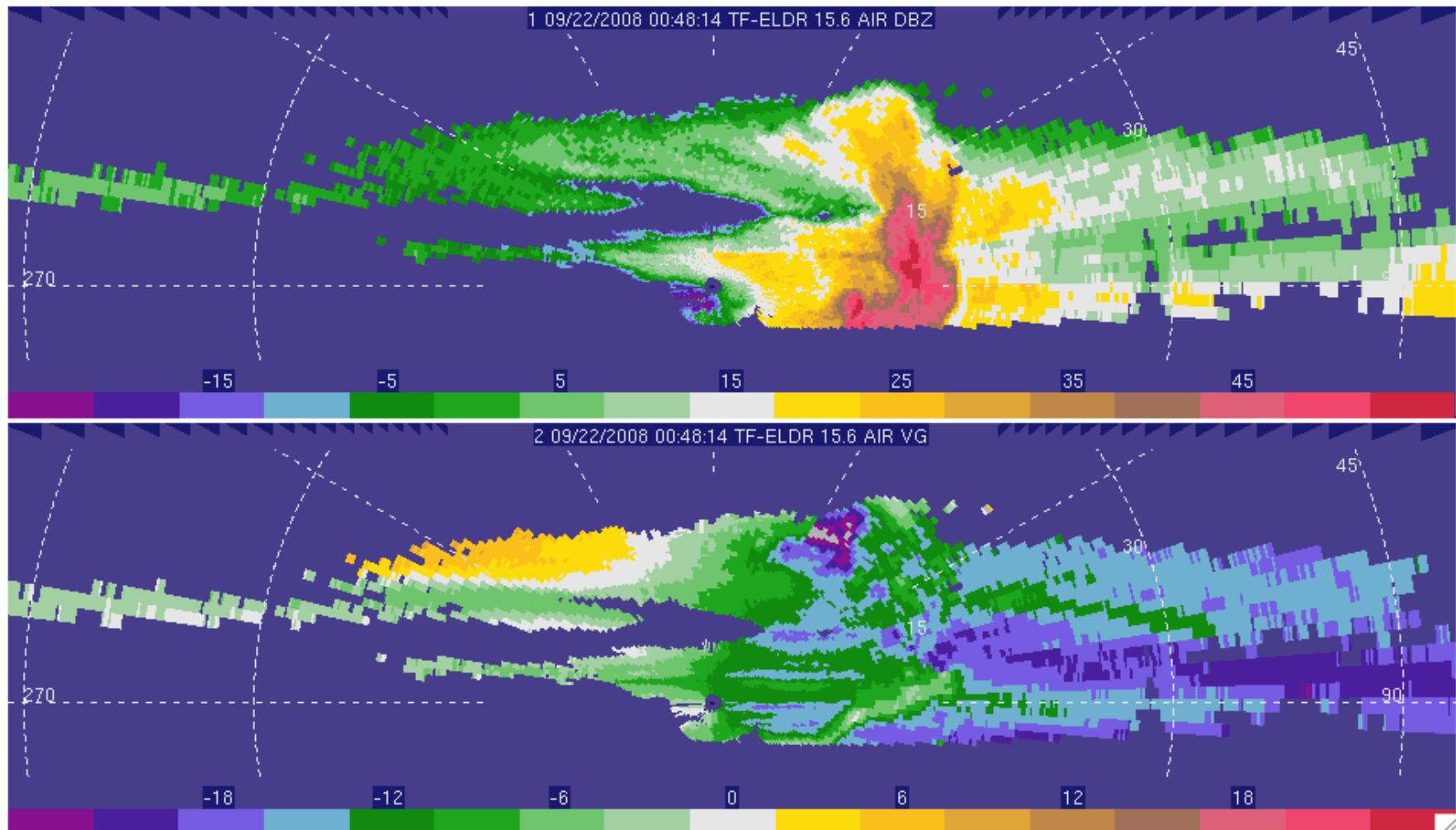
= Text File

1. \*Translate the raw ELDORA field format data into DORADE sweep files
2. \*Calculate navigation correction factors (cfac files) for each flight
3. *Fine-tune navigation corrections for each leg of data*
4. **Edit the data to remove ground echo, noise, clutter, and radar side-lobes, as well as velocity unfolding.**
5. **Interpolate and/or Synthesize multiple data files to get 3-dimensional wind field and derived quantities.**

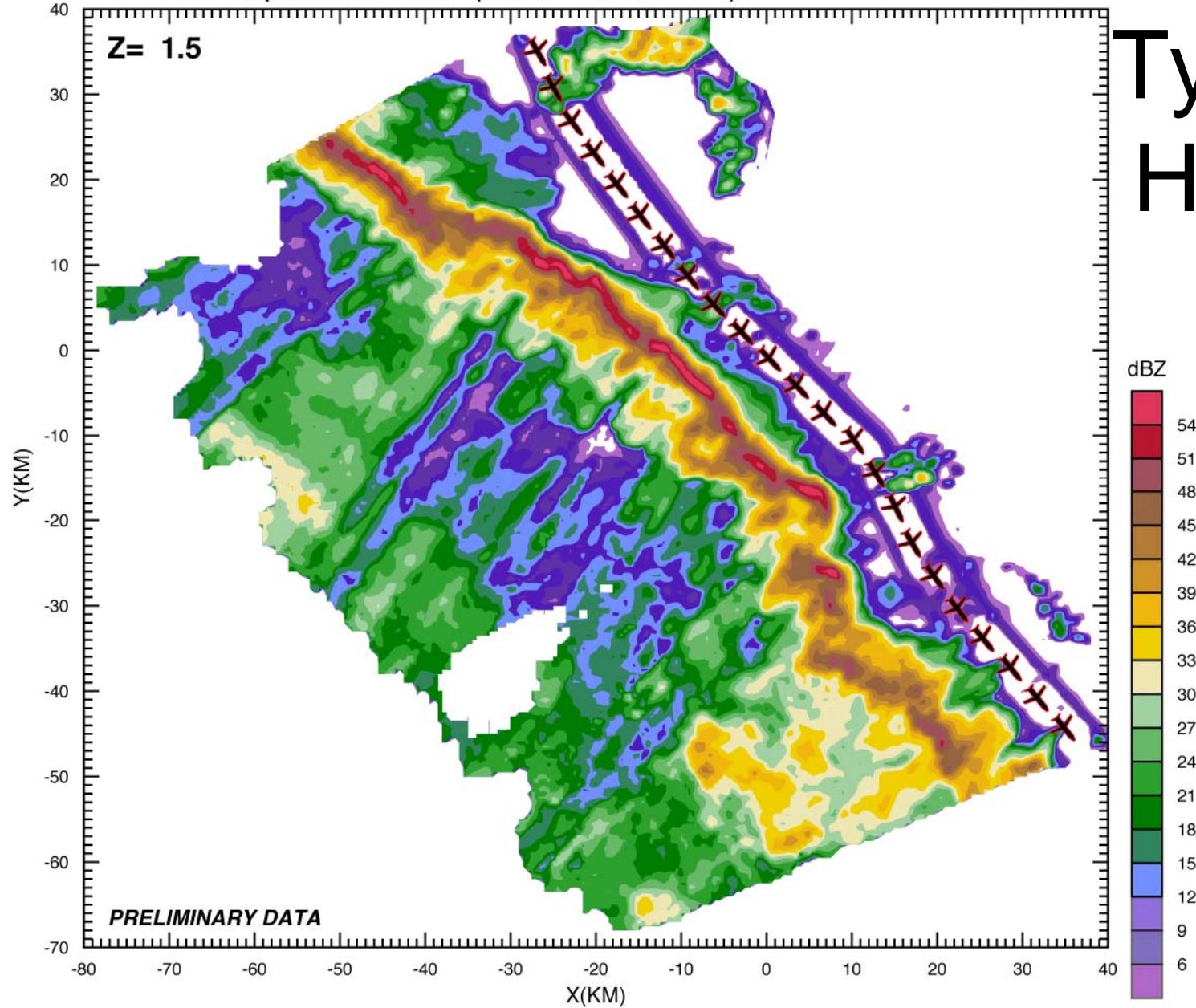
# Raw Data



# Edited Data

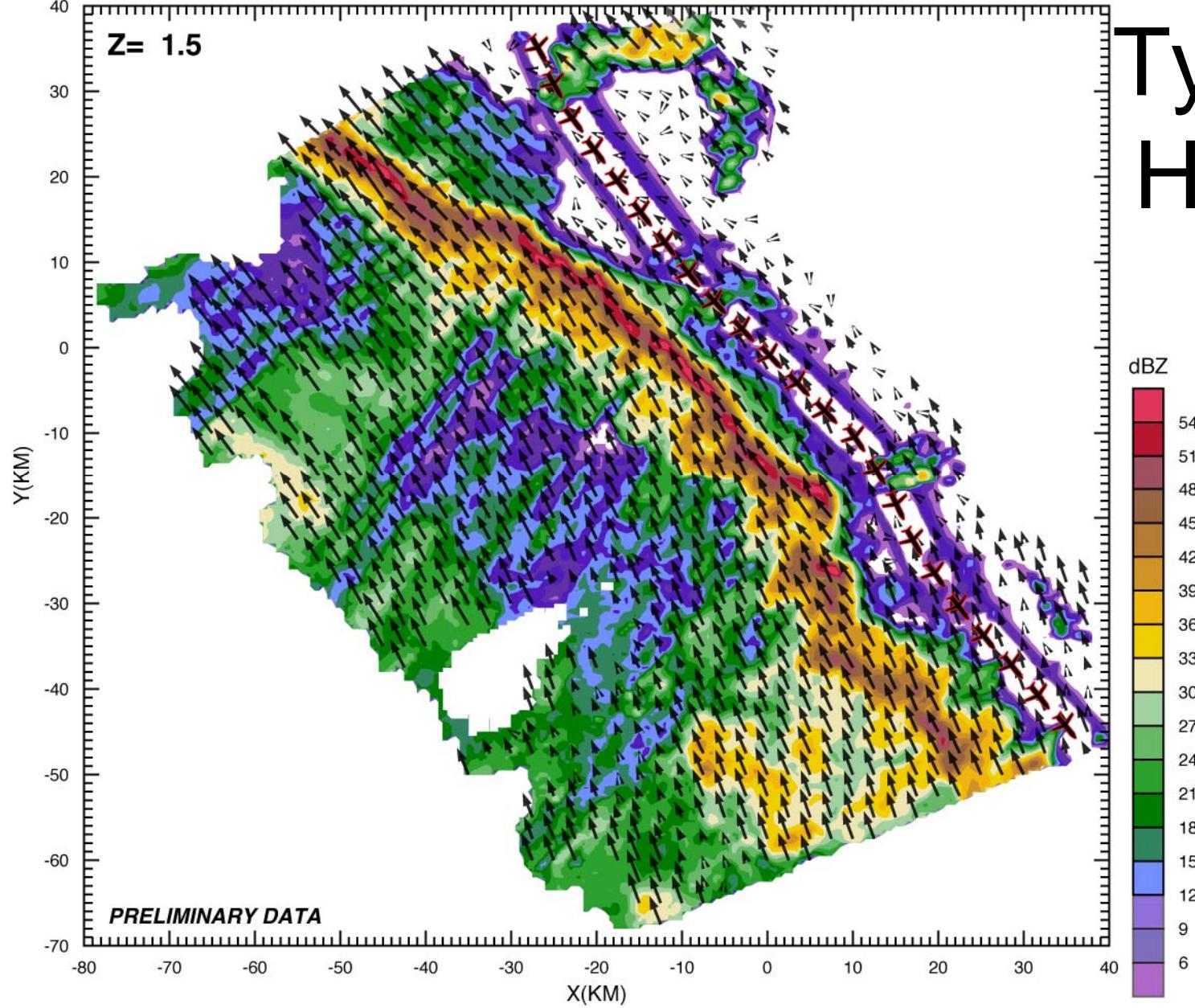


RF17 22 September 2008 (0040 - 0058 UTC)



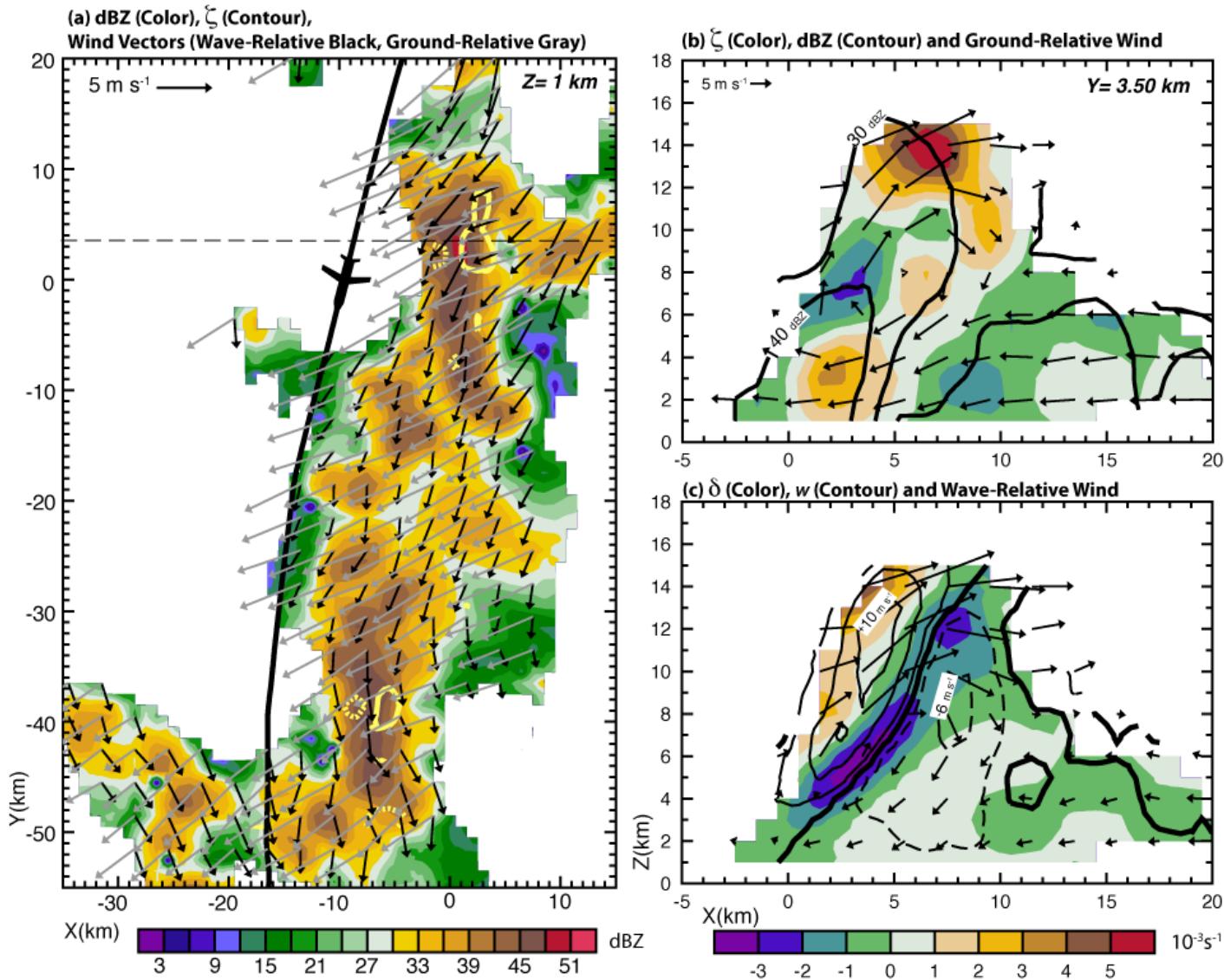
# Typhoon Hagupit

RF17 22 September 2008 (0040 - 0058 UTC)



Typhoon  
Hagupit

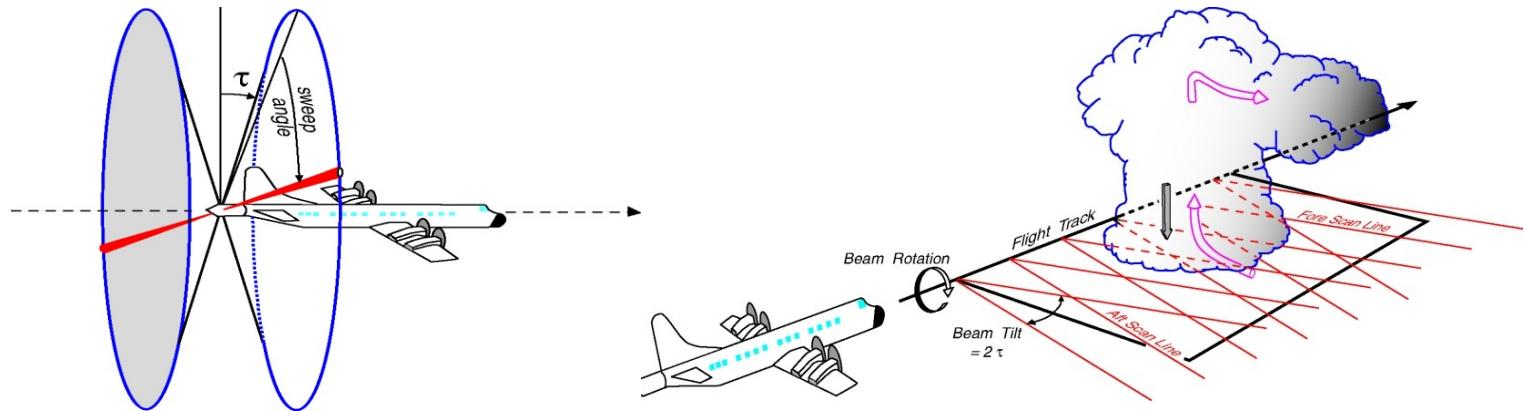
# Hagupit Pre-genesis



# Multi-Doppler Synthesis

$$V_r = u \sin(a) \cos(e) + v \cos(a) \cos(e) + (w + w_t) \sin(e)$$

$$\begin{pmatrix} \sin^2 a \cos^2 e & \sin a \cos a \cos^2 e & \sin a \cos a \sin e \\ \sin a \cos a \cos^2 e & \cos^2 a \cos^2 e & \cos a \cos a \sin e \\ \sin a \cos a \sin e & \cos a \cos a \sin e & \sin^2 e \end{pmatrix} \begin{pmatrix} u \\ v \\ w + w_t \end{pmatrix} = \begin{pmatrix} V_r \sin a \cos e \\ V_r \cos a \cos e \\ V_r \sin e \end{pmatrix}$$



# Doppler Synthesis Approaches

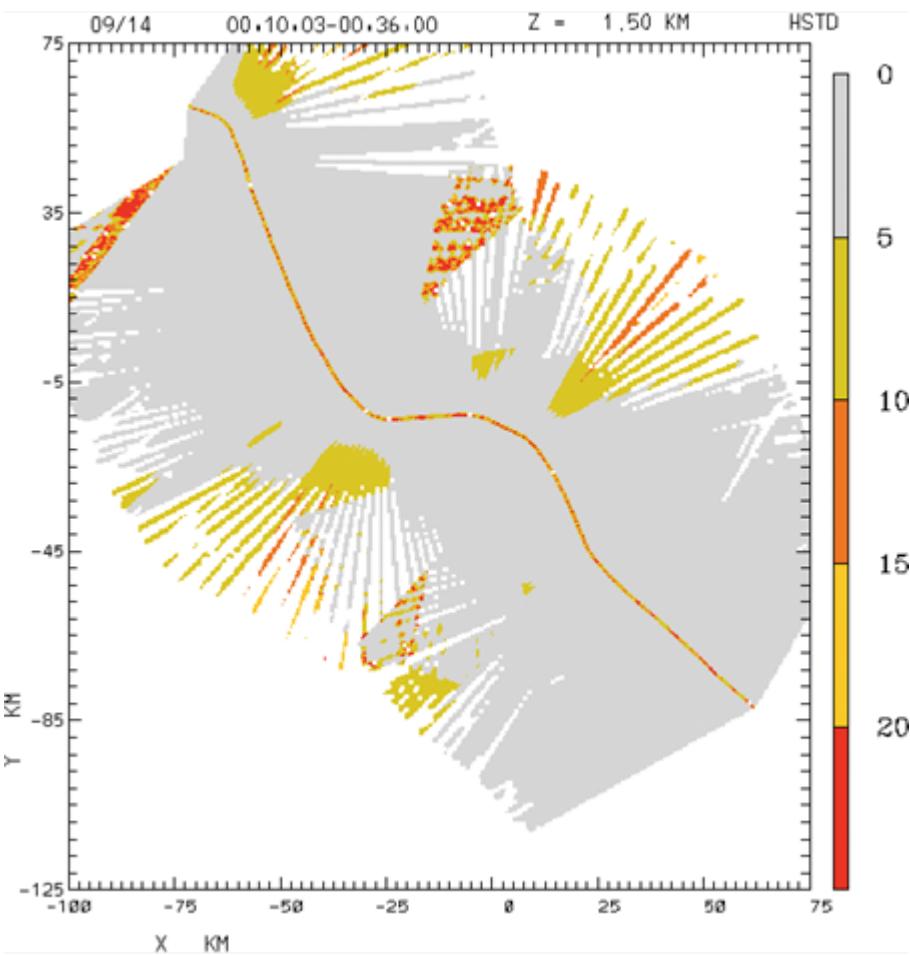
- **Forward Local** (Sprint/Reorder & Cedric)
  - Empirical Interpolation of  $V_r$  (Distance weighted averaging), then local synthesis
- **Forward Global** (Gamache, Raymond & Carrillo\*)
  - Empirical Interpolation, then global synthesis
- **Reverse Global** (Gao et al. 1999/2004, Bell)
  - Interpolation from grid to radar space during cost function minimization

# ‘Forward Local’ synthesis

- ‘Conventional’ using reorder/cedric
- Quasi-horizontal assumption
- Resolve horizontal velocities then integrate continuity equation vertically to obtain vertical velocities
- Limited to elevation angle less than 45 deg
- Difficult to resolve storm top when storm is close to the radar

# Problems with Radial Velocity Interpolation and Averaging

- Big issue for airborne synthesis and Reorder
- Also a problem for ground-based platforms near the radar
- Solutions:
  - Use more, small chunks
  - Include full az/elev info
  - Avoid it



3-D Variational Formulation (Gamache 1997, Reasor et al 2009): Solve two or more radial velocity equations and mass continuity equation simultaneously.

$$F = \lambda_1 J_1 + \lambda_2 J_2 + \cdots + \lambda_n J_n + \lambda_{n+1} J_{n+1} + \lambda_{n+2} J_{n+2} + \lambda_{n+3} J_{n+3}$$

$$J_m = \sum_{l=1}^L \sum_{k=1}^K \sum_{j=1}^J \sum_{i=1}^I \rho_k (V_{rml} - u_{ijk} \cos \theta_{ml} \cos \phi_{ml} - v_{ijk} \sin \theta_{ml} \cos \phi_{ml} - w_{ijk} \sin \phi_{ml} - v_{Tml} \sin \phi_{ml})^2 \alpha_{ijkl}$$

$$J_{n+1} = \sum_{k=1}^K \sum_{j=1}^J \sum_{i=1}^I (\nabla \cdot \rho_k \vec{V}_{ijk})^2$$

$$\begin{aligned} J_{n+2} = & \sum_{k=1}^K \sum_{j=1}^J \sum_{i=1}^I \left\{ \left( \frac{\partial^2 \rho u_{ijk}}{\partial x^2} \right)^2 + \left( \frac{\partial^2 \rho u_{ijk}}{\partial y^2} \right)^2 + \left( \frac{\partial^2 \rho u_{ijk}}{\partial z^2} \right)^2 + \left( \frac{\partial^2 \rho v_{ijk}}{\partial x^2} \right)^2 + \left( \frac{\partial^2 \rho v_{ijk}}{\partial y^2} \right)^2 + \left( \frac{\partial^2 \rho v_{ijk}}{\partial z^2} \right)^2 \right. \\ & + \left( \frac{\partial^2 \rho w_{ijk}}{\partial x^2} \right)^2 + \left( \frac{\partial^2 \rho w_{ijk}}{\partial y^2} \right)^2 + \left( \frac{\partial^2 \rho w_{ijk}}{\partial z^2} \right)^2 + \left( \frac{\partial^2 \rho u_{ijk}}{\partial x \partial y} \right)^2 + \left( \frac{\partial^2 \rho u_{ijk}}{\partial x \partial z} \right)^2 + \left( \frac{\partial^2 \rho v_{ijk}}{\partial y \partial z} \right)^2 \\ & \left. + \left( \frac{\partial^2 \rho v_{ijk}}{\partial x \partial y} \right)^2 + \left( \frac{\partial^2 \rho v_{ijk}}{\partial x \partial z} \right)^2 + \left( \frac{\partial^2 \rho w_{ijk}}{\partial y \partial z} \right)^2 + \left( \frac{\partial^2 \rho w_{ijk}}{\partial x \partial y} \right)^2 + \left( \frac{\partial^2 \rho w_{ijk}}{\partial x \partial z} \right)^2 + \left( \frac{\partial^2 \rho w_{ijk}}{\partial y \partial z} \right)^2 \right\} \end{aligned}$$

$$J_{n+3} = \sum_{k=1}^K \sum_{j=1}^J \sum_{i=1}^I \rho_k (w_{ijk} - w_B)^2 \delta_B$$

# TCVAR (Bell 2009)

$$J(q) = \frac{1}{2}q^T q + \frac{1}{2}(\mathbf{H}\mathbf{C}q - d)^T \mathbf{R}^{-1}(\mathbf{H}\mathbf{C}q - d)$$

$$\nabla J(q) = (\mathbf{I} + \mathbf{C}^T \mathbf{H}^T \mathbf{R}^{-1} \mathbf{H} \mathbf{C})q - \mathbf{C}^T \mathbf{H}^T \mathbf{R}^{-1} d$$

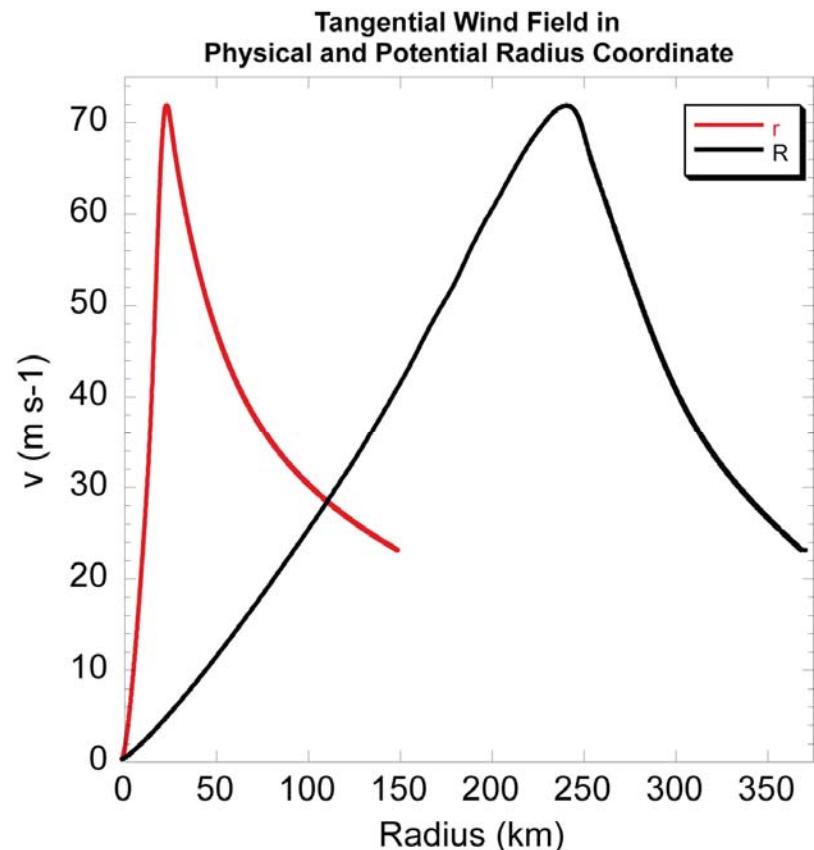
$$\mathbf{B} = \sqrt{\mathbf{B}}^T \sqrt{\mathbf{B}} = \mathbf{C}^T \mathbf{C}$$

$$q = \mathbf{C}^{-1} \delta x = \mathbf{C}^{-1} (x - x_b)$$

$$\mathbf{C} = \mathbf{PSDF}$$

**P** = Physical Coordinate Transform  
**S** = Cubic Spline Transform  
**D** = Diagonalized Background Error  
**F** = Recursive Gaussian Filter

- Can combine radar, dropsonde, and flight level data
- Low noise via cubic interpolations and spectral derivatives
- Tunable error specifications and filtering



$$q(r,z) = \{\rho, rv, \psi, h, q'_v, \rho'_a\}$$

# Raymond & Carrillo

# Advantages / Disadvantages

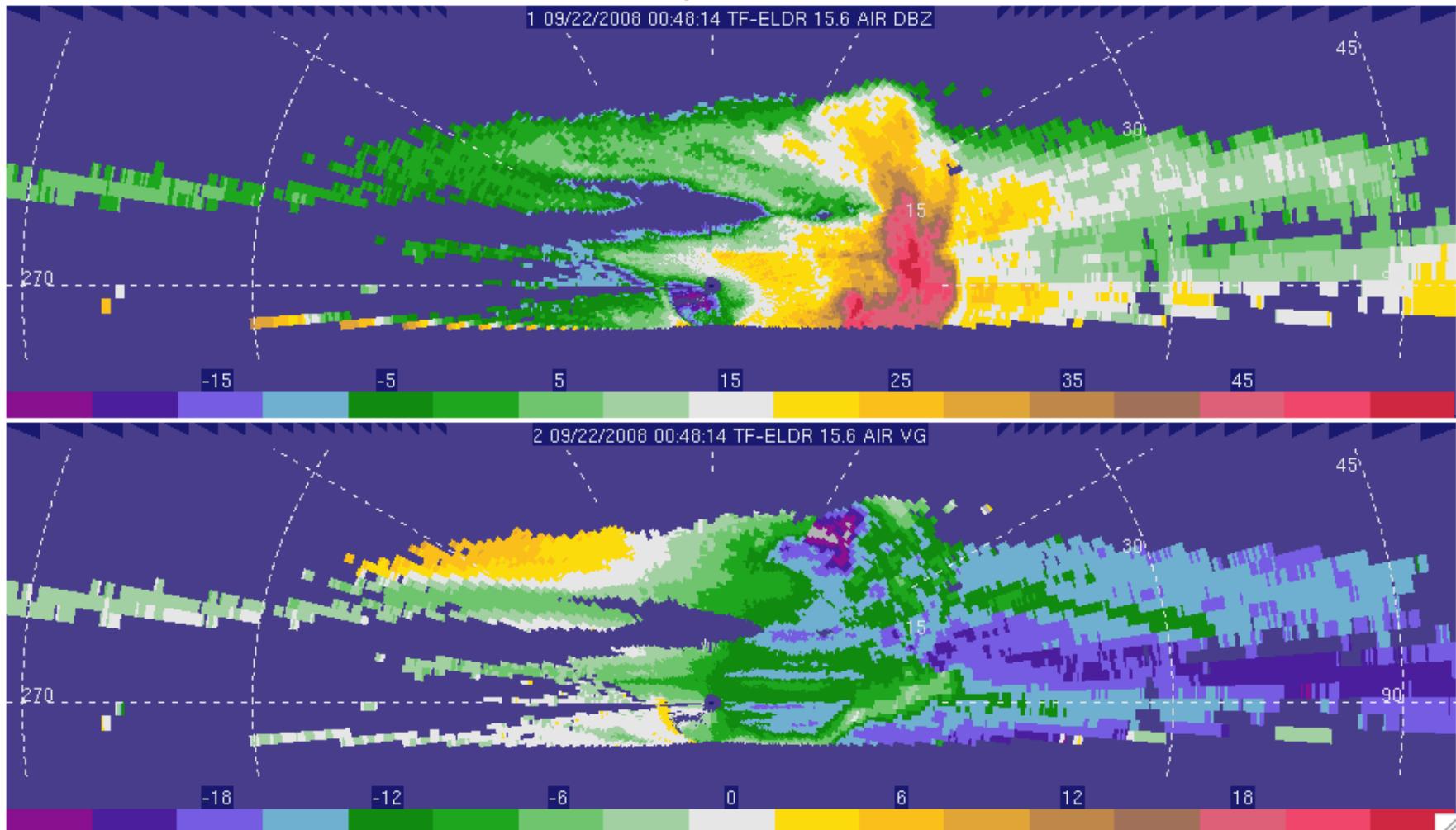
	Error Propagation	Memory/CPU	Diagnostics	Multiple Data Sources	Anisotropic Filtering	Extra Balance Constraints
Forward Local	Vertical	Low/Fast	Established	Difficult	Possible	Difficult
Forward Global	Horizontal & Vertical	High/Slow	Complex	Possible	Difficult	Possible
Reverse Global (Bell)	BG Error Covariance	Low/Slow	Moderate	Yes	Yes	Possible

Multiple analysis techniques are a good thing!

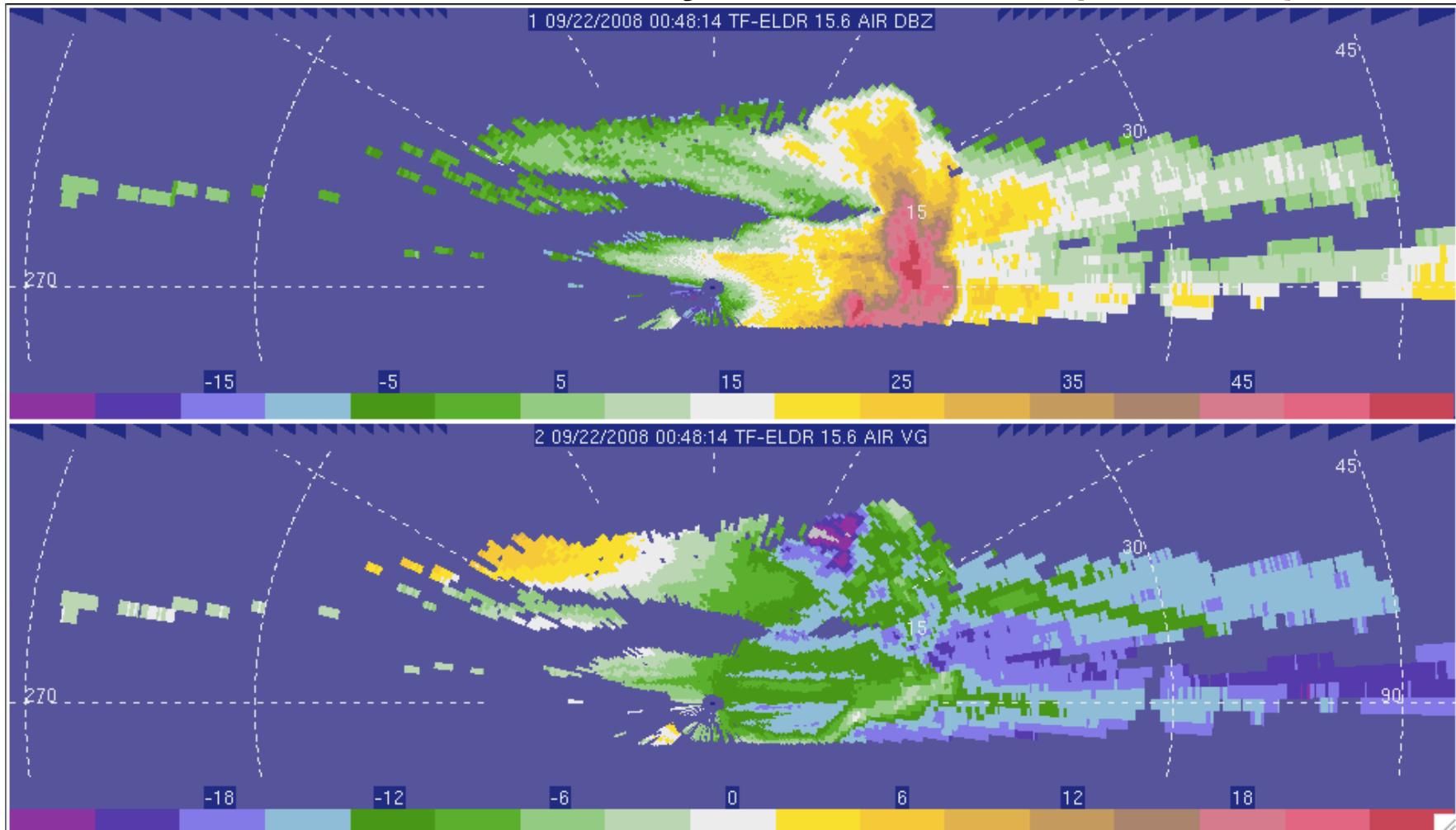
# Automatic Editing for Data Assimilation and New Users

- Still work in progress
  - Fuzzy logic echo classification system under development
- Soloii scripts available now for light (80%) to heavy (99%) artifact removal
  - In between is most difficult

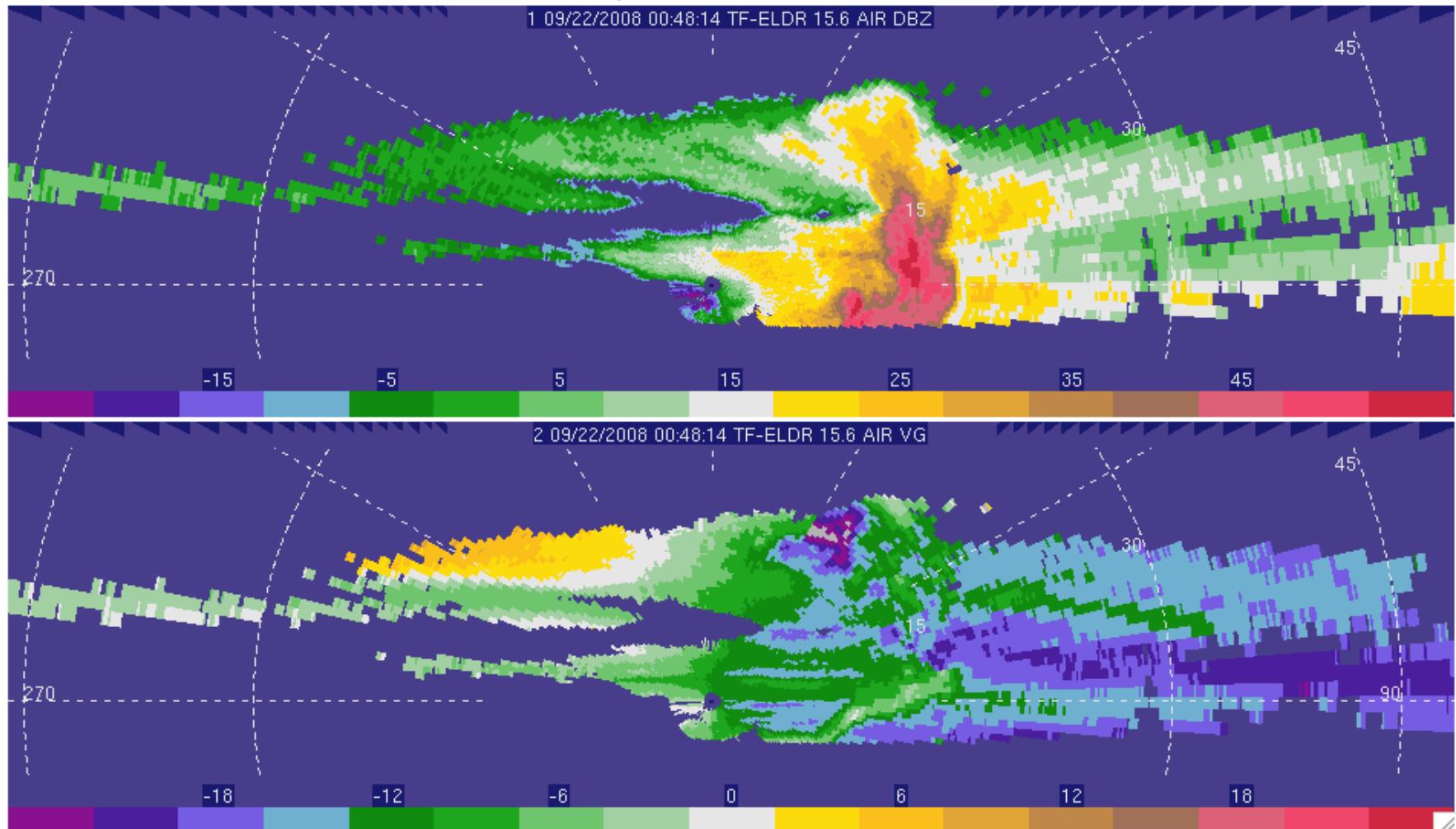
# Automatically Edited (80%)



# Automatically Edited (99%)



# Manually Edited Data



# Summary

- Data quality is good with exception of aft reflectivity later in project.
- Radar data is ready, on CODIAC soon
  - CAPPI movies will be available soon also
- A variety of software tools are available for viewing, editing, and processing
- New users welcome! Come talk to us about how you could use ELDORA data